



REPORT

STRUCTURAL AND CIVIL ENGINEERS

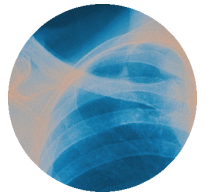
AYRBURN FARM INFRASTRUCTURE REPORT

PREPARED FOR

AYRBURN FARM DEVELOPMENTS LTD

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Ayrburn Farm Infrastructure Report

Prepared For:

Ayrburn Farm Developments Ltd

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Prepared By:

A handwritten signature in black ink, appearing to be 'AJ' followed by a horizontal line.

Andrea Jarvis
PROJECT DIRECTOR

Holmes Consulting Group LP

www.holmesgroup.com

Queenstown

T: +64 (03) 441 3055

Reviewed By:

A handwritten signature in black ink, appearing to be 'J.T.' followed by a horizontal line and a dot.

John Trowsdale
PROJECT DIRECTOR

OFFICES IN:

Auckland

Hamilton

Wellington

Christchurch

Queenstown

San Francisco



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INTRODUCTION

Holmes Consulting Group LP have been engaged by Ayrburn Farm Developments Ltd to complete an infrastructure report as an addendum to the report completed by Clark Fortune McDonald & Associates (CFMA) in February 2015.

Ayrburn Farm is a development proposed to the north of Lake Hayes, south of Millbrook, in the Queenstown Lakes District. The wider site is 45 Ha in area, with Mill Creek passing through the lower lying portions of the site.

CFMA's report covered a proposed 150 lot residential special housing area (SHA) development. Modelling of the water and wastewater networks by Tonkin & Taylor Ltd (T&T) and Rationale Ltd (Rationale) respectively was also based on 150 residential lots.

The current proposal, which this report is based on, is for a 191 lot retirement village, plus associated care facilities and 10 houses for employees.

SCOPE OF WORK

The scope of work for this project included the following:

1. Assess the expected infrastructure demand as a result of the change in proposed use since initial reports were completed.
2. Review existing reports from CFMA, Rationale and T&T and provide comment on the assessments undertaken.
3. Report on the feasibility of servicing the development, to support an SHA application.
4. Report on required upgrades to the wider infrastructure networks.

LIMITATIONS

Findings presented as a part of this project are for the sole use of Ayrburn Farm Developments Ltd and Queenstown Lakes District Council in their evaluation of the subject properties. The findings are not intended for use by other parties, and may not contain sufficient information for the purposes of other parties or other uses. Our assessments are based on a desk study only.

Our professional services are performed using a degree of care and skill normally exercised, under similar circumstances, by reputable consultants practicing in this field at this time. No other warranty, expressed or implied, is made as to the professional advice presented in this report.



BASIS OF ASSESSMENT

As noted above, the existing reports have assessed a 150 lot residential SHA. The current proposal comprises 191 retirement village lots, 10 houses for employees and associated communal and care facilities.

The residential lots were assessed based on an average of 3 people per lot, resulting in a total population of 450 people. By empirical measure, the number of people per unit in retirement villages is approximately 1.3 people per unit for a newly populated village, regardless of the number of rooms in each unit. This then drops over time and stabilises around 1.1 people per unit. Based on the more conservative 1.3 people per lot for the retirement village lots and 3 people per house for the employee houses, the total population for the retirement village proposal is approximately 280 people. The new proposal is therefore less intensive and the modelling reports are assumed to be conservative.

WASTEWATER

The demands on the wastewater network have been assessed by Rationale based on 450 people, at an average loading of 245 litres/person/day. This is based on the standard 735 litres/connection/day (3 people/connection) utilised in the Wakatipu dynamic wastewater model. The applied dry weather peaking factor is 2.1, and 45.9 Ha of catchment has been applied for wet weather/infiltration effects.

The site as a whole is 45.9 Ha. As the proposal shows 31.7 Ha (approximately 69% of the site) will be retained for farm use in perpetuity, the infiltration loading assumed by Rationale is considered very conservative.

Clause 5.3.5.1 of QLDC's Land Development and Subdivision Code of Practice refers to average dry weather flows of 250 litres/person/day, a dry weather peaking factor of 2.5 and a dilution/infiltration factor of 2 for wet weather.

Based on the revised population of 280 noted above, the average dry weather flow based on the Land Development and Subdivision Code of Practice is approximately 0.8 l/s, with a peak wet weather flow of 4.05 l/s. This is significantly lower than the 8.5 l/s assumed by Rationale.

Rationale's modelling report concluded that the existing infrastructure has adequate capacity for the formerly proposed 150 lot subdivision, with the exception of Lake Hayes Pump Station 1 (PS1), the rising main from this pump station and portions of the network between PS1 and Lake Hayes Pump Station 2 (PS2).

PS1 currently has a duty pump capacity of 2.6 l/s. The current day maximum flow is 5 l/s, and future day maximum inflow (without this development) is assessed as 6 l/s. Due to this current shortfall in capacity, PS1 is due for upgrade, even if the proposed



development were not to proceed. The additional 4.05 l/s from this development makes this upgrade more critical and increases the scale of the upgrade required.

Upgrades to this pump station are therefore required to service the existing catchment, and therefore by definition to also service this development. Pump upgrades and either emergency storage or an emergency standby generator will be required to meet the requirements of the QLDC infrastructure code.

The rising main from this pump station is currently 100 mm PVC. Rationale recommend this is upgraded to 150 mm diameter, however this is based on a required duty pump capacity of 16 l/s. Based on the comments around total dynamic head in the Rationale report, it is expected that at the reduced demand flows described above, the rising main upgrade will not be required, as velocities would be closer to 1.3 m/s, which is acceptable.

Two overflows within the gravity network between PS1 and PS2 are identified in the Rationale report. The volumes of these overflows are 38.5 m³ and 0.7 m³ respectively, based on the situation as modelled. The reduced demand flows described above are expected to reduce these overflows, and potentially eliminate them. It is recommended that further modelling is undertaken to confirm this, however it is noted that 150 mm PVC sewer lines laid to minimum falls as per NZS4404:2010 requirements can cater for 13.05 l/s of flow.

It is therefore concluded that the required upgrades to the wastewater infrastructure to support this development are only those associated with PS1 (which largely are required by the catchment already); that is, the pump upgrades and either emergency storage or generation.

WATER SUPPLY

As per the wastewater modelling, the water supply modelling has been carried out based on 150 residential lots. The resulting total population of 450 people with an average day demand of 700 l/person/day (as per clause 6.3.5.6 of QLDC's Land Development and Subdivision Code of Practice) has been considered.

The revised population of 280 people as described above generates an average daily flow water demand of 2.27 l/s, compared to the 3.65 l/s modelled by T&T. The peak hour flow of 14.98 l/s is similarly well below the 24.1 l/s modelled. The assessments by T&T are therefore considered conservative.

T&T have modelled this domestic demand, in addition to considering the fire flow requirements. They have assumed a fire hazard category of FW2 for the previously proposed residential lots, and also assessed whether an FW3 supply can be provided to the previously proposed retail centre. The retail centre was proposed for the same general location as the care facilities, restaurant and office are now proposed.



Assuming the maximum fire cell size is no larger than 599 m², an FW3 classification is still considered valid for these activities.

T&T have assumed that Lake Hayes Estate will be supplied by the Shotover Country water supply bores, and therefore conclude that adequate flows and pressures are available to service the development from the Lake Hayes Water Scheme. This will require a 150 mm internal diameter main as an extension to the network along Arrowtown-Lake Hayes Road (a distance of approximately 300 m), connecting to an internal reticulation network within the development. To provide fire flows to the care facilities precinct, this 150 mm ID main will need to extend through to the area within the site. If these facilities are sprinklered, it may be possible to decrease the size of the internal main for part of its length.

Due to the maximum elevation difference between the Lake Hayes reservoir and the development of 95 m, a pressure reducing valve within the development will be required to limit pressures to the maximum allowable 900 kPa.

Other than the water main extension described above, no upgrades to the wider water network are required to support the development.

STORMWATER DEMANDS

Stormwater runoff generated has not been modelled, or assessed by CFMA in their original infrastructure report. General comments indicate that the intention is to discharge stormwater to Mill Creek within the site, which eventually discharges into Lake Hayes. Discharges within the Lake Hayes catchment generally require specific design, and consideration by Otago Regional Council to determine whether a resource consent is required. It is likely that any discharges to Mill Creek will require both treatment to remove potential contaminants and attenuation/detention to limit outflows to the pre-development flows.

The site is currently in pasture, with an associated stormwater run-off coefficient of 0.3. Although the final site coverage is unable to be determined at this stage, it is estimated that a run-off coefficient of 0.65 (as defined in the New Zealand Building Code clause E1 for “Industrial, commercial, shopping areas and town house developments”) is appropriately conservative. This has been applied to the development area of 14.2 Ha; the area to remain as pasture has not been considered.

As per QLDC’s Land Development and Subdivision Code of Practice, a return interval of 20 years has been chosen. A duration of 10 minutes (considered conservative) has been adopted for the post-development flows, and 20 minutes for the pre-development flows. From NIWA’s HIRDS database, this translates to rainfall intensities of 36 mm/hour (post-development) and 27.3 mm/hour (pre-development).



Based on the Rational Method, run-off rates for the pre-development and post-development situations are as follows:

$$Q = CIA/360$$

$$Q \text{ (pre-development)} = 0.3 \times 27.3 \times 14.2 / 360 = 0.323 \text{ m}^3/\text{s}$$

$$Q \text{ (post-development)} = 0.65 \times 36 \times 14.2 / 360 = 0.923 \text{ m}^3/\text{s}$$

The volume of storage required will require specific design, however this will likely be provided within a constructed wetland or pond system. Roadside swales instead of piped infrastructure is theoretically possible, as is on-site soakage to ground for each lot, but not considered feasible for this development due to the small lot sizes and reduced road reserve widths.

CONCLUSIONS

The proposed retirement village is able to be serviced by the surrounding water supply and wastewater networks, subject to upgrades to Lake Hayes Wastewater Pump Station 1 (which are required in any event, albeit to a slightly lesser degree, to cater for the demand associated with existing development in the catchment), and installation of a new water main from the intersection of Speargrass Flat Road and Arrowtown-Lake Hayes Road through to the development.

The proposed retirement village development will place lower demands on the surrounding infrastructure than the previously assessed 150 lot residential development would have. This reduced demand has the potential to reduce the scope of off-site upgrade works required, as described above.

The specific upgrades required are as follows:

- Upgrade the pumps within PS1 to provide minimum duty pump capacity of 10.05 l/s. The pumps are currently able to cater for 2.6 l/s, and without this development, 6 l/s to cater for future demands is required. The costs associated with this would therefore be split between QLDC and the developer, with approximately 54 % of the required additional capacity attributed to this development.
- Provide either emergency storage or a standby generator for PS1. Due to the proximity to Lake Hayes and the probability of high groundwater at this location, it is recommended that a standby generator, appropriately screened to reduce visual impact, would be a more cost effective solution at this site.
- Install a new 150 mm ID water main along Arrowtown-Lake Hayes Road, with a length of approximately 300 m.



The internal infrastructure for the site will require detailed design, and should include stormwater treatment and attenuation, and extension of the 150 mm ID water main through to the central care and communal facilities precinct.